

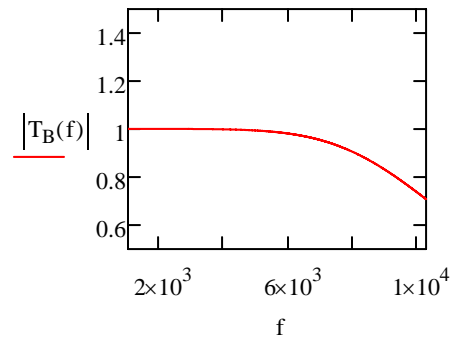
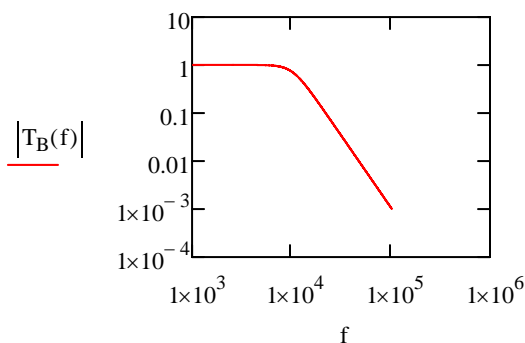
ECE 3042 Experiment 6 Active Filter Design

- Design a 3rd order Butterworth low-pass filters having a dc gain of unity and a cutoff frequency, f_c , of 10.28 kHz.

$f_c := 10.28\text{kHz}$ $K := 1$ The transfer function is given on page 72 $j := \sqrt{-1}$

$$T_B(f) := K \cdot \frac{1}{j \cdot \frac{f}{f_c} + 1} \cdot \frac{1}{\left(j \cdot \frac{f}{f_c} \right)^2 + j \cdot \frac{f}{f_c} + 1}$$

This is the product of a 1st order LPF & 2nd order LPF.



To implement this with a circuit cascade the circuit on page 82 with that on page 83. For each the dc gain is unity (K) which means that RF is zero (a wire) and the resistor from the inverting input to ground is infinity (nothing there).

Start by picking two of the capacitors to be $0.01 \mu\text{F}$. For the Butterworth filter ω_c & ω_o are the same.

So for the circuit on page 82 $C := 0.01 \mu\text{F}$ $R_1 := \frac{1}{2 \cdot \pi \cdot f_c \cdot C}$ $R_1 = 1.548 \times 10^3 \Omega$
 This is a 1st order LPF

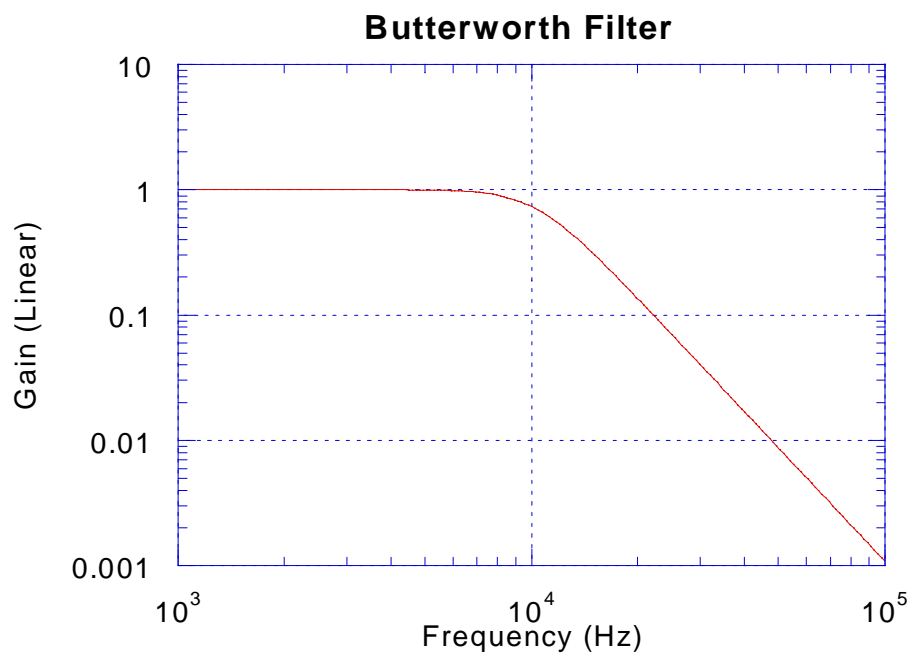
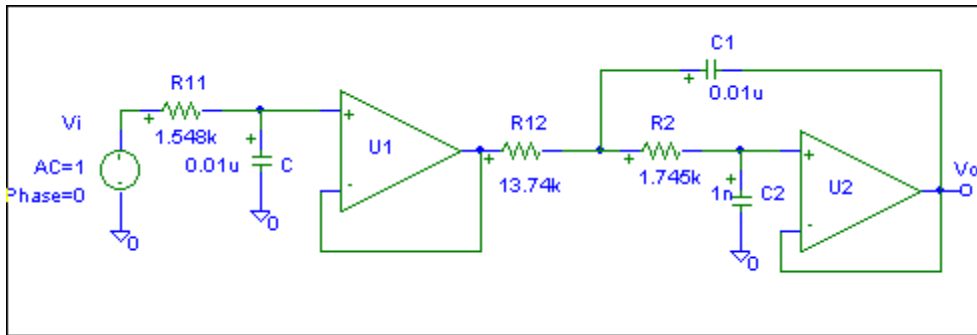
For the circuit shown on page 83, the 2nd order LPF, pick $C_1 := 0.01 \mu\text{F}$ $C_2 := 0.1 C_1$
 then Eq. 6.84 applies with $Q=1$ and $\omega_o = \omega_c$ $Q := 1$ $\omega_o := 2 \cdot \pi \cdot f_c$

$$R_1 := \frac{1}{2 \cdot Q \cdot \omega_o \cdot C_2} \cdot \left(1 + \sqrt{1 - 4 \cdot Q^2 \cdot \frac{C_2}{C_1}} \right)$$

$$R_2 := \frac{1}{2 \cdot Q \cdot \omega_o \cdot C_2} \cdot \left(1 - \sqrt{1 - 4 \cdot Q^2 \cdot \frac{C_2}{C_1}} \right)$$

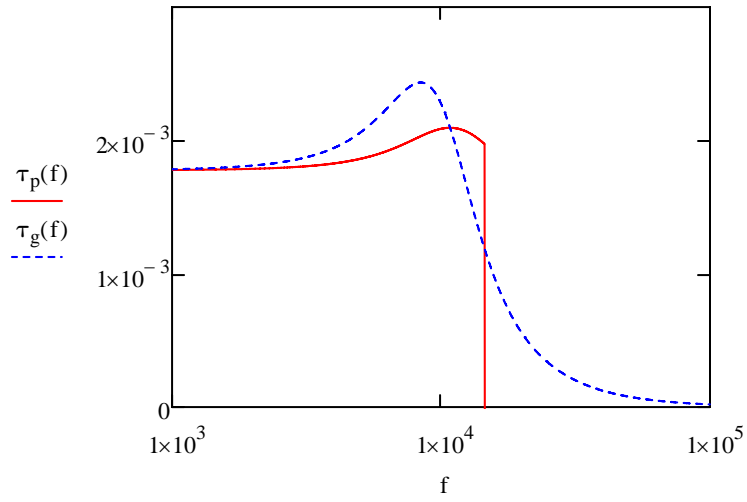
$R_1 = 1.374 \times 10^4 \Omega$ $R_2 = 1.745 \times 10^3 \Omega$ $C_1 = 1 \times 10^{-8} \text{F}$ $C_2 = 1 \times 10^{-9} \text{F}$

Now that all of the component values have been determined it's time to simulate it with SPICE



The next step is to head to the lab and build the circuits. Use 741s, LF351s, LF347s. The resistors for your use are 5%. The caps are 20%. Try to find 3 caps reasonably close to the design values.

$$\varphi(f) := \frac{180}{\pi} \cdot \arg(T_B(f)) \quad \tau_p(f) := \frac{-1}{2 \cdot \pi} \cdot \frac{\varphi(f)}{f} \quad \tau_g(f) := \frac{-1}{2 \cdot \pi} \cdot \left(\frac{d}{df} \varphi(f) \right)$$



2. Design a 3rd order unity dc gain Chebyshev LPF with a -3 frequency of 10.28 kHz and 0.5 db ripple in the pass band.

$$\text{db} := 0.5 \quad f_3 := 10.28 \text{ kHz} \quad K := 1 \quad n := 3 \quad t_3(x) := 4 \cdot x^3 - 3 \cdot x \quad j := \sqrt{-1}$$

$$\epsilon := \sqrt{10^{\frac{\text{db}}{10}} - 1}$$

Eq. 6.47 must be solved to obtain the relationship between ω_c & ω_3 which requires that Eq. 6.46 be solved which is a cubic polynomial $g(x)$

$$g(x) := 4 \cdot x^3 - 3 \cdot x - \frac{1}{\epsilon}$$

Since $t_3(0)=0$ To solve this form the vector v

$$v := \begin{pmatrix} -1 \\ \epsilon \\ -3 \\ 0 \\ 4 \end{pmatrix}$$

This is done with the Insert Matrix selection from the toolbar. The roots are now obtained with the polyroots(.) function. With MathCad the index on arrays in a matrix begin with 0.

Since this is a cubic polynomial it will have at least one real root and its the one required.

$$u := \text{polyroots}(v) \quad u = \begin{pmatrix} -0.584 - 0.522i \\ -0.584 + 0.522i \\ 1.167 \end{pmatrix} \quad x := u_{2,0} \quad x = 1.167$$

$$f_c := \frac{f_3}{x} \quad f_c = 8.805 \times 10^3 \frac{1}{s}$$

The transfer function is Eq. 6.56 which requires h , a_2 , a_1 , & b_1

$$h := \tanh\left(\frac{1}{n} \cdot \text{asinh}\left(\frac{1}{\epsilon}\right)\right) \quad \epsilon = 0.349 \quad h = 0.531 \quad \theta_1 := \frac{1}{3} \cdot \frac{\pi}{2}$$

$$a_2 := \frac{h}{\sqrt{1-h^2}} \quad a_1 := \sqrt{\frac{1}{1-h^2} - (\sin(\theta_1))^2} \quad b_1 := \frac{1}{2} \cdot \sqrt{1 + \frac{1}{(h \cdot \tan(\theta_1))^2}}$$

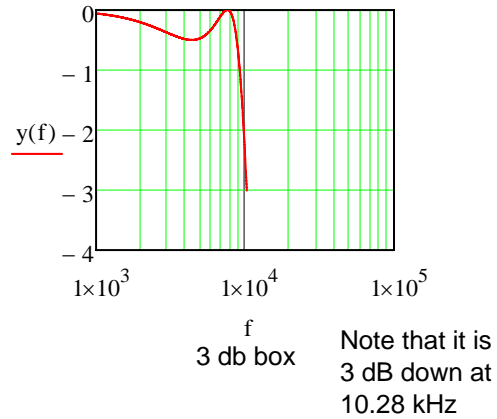
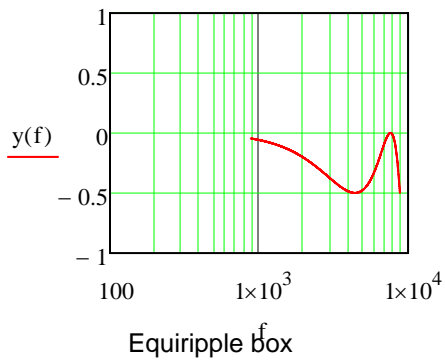
$$a_2 = 0.626 \quad a_1 = 1.069 \quad b_1 = 1.706$$

The transfer function then becomes

$$T_C(f) := K \cdot \frac{1}{\frac{j \cdot f}{a_2 \cdot f_c} + 1} \cdot \frac{1}{\left[\left(\frac{j \cdot f}{a_1 \cdot f_c} \right)^2 + \frac{1}{b_1} \cdot \frac{j \cdot f}{a_1 \cdot f_c} + 1 \right]}$$

$$y(f) := 20 \cdot \log(|T_C(f)|)$$

For a check of the solution the magnitude of the transfer function in db will be plotted vs f



Now the circuit must be designed. This requires a 1st order lpf cascaded with a 3rd order lpf. This can be done by cascading the circuit shown in Fig. 6.9.a (page 83) with Fig. 6.11 (page 83).

For the 1st order filter, since the dc gain is unity, $K=1$, pick $R_F=0$ (a wire) and R_1 infinity.

Pick $C_1 := 0.01 \mu\text{F}$

$$R_1 := \frac{1}{2 \cdot \pi \cdot a_2 \cdot f_c \cdot C_1} \quad R_1 = 2.885 \times 10^3 \Omega$$

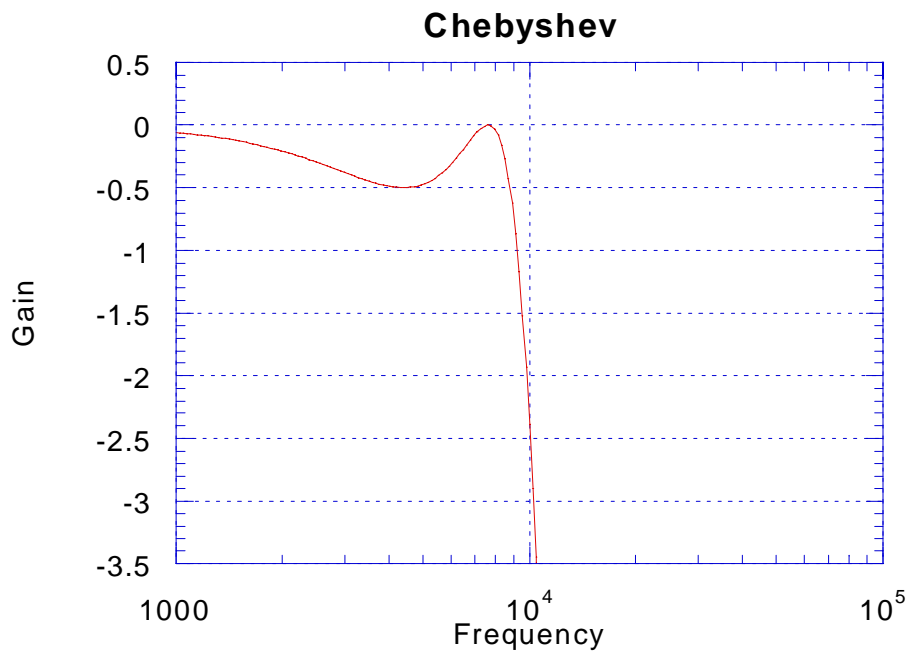
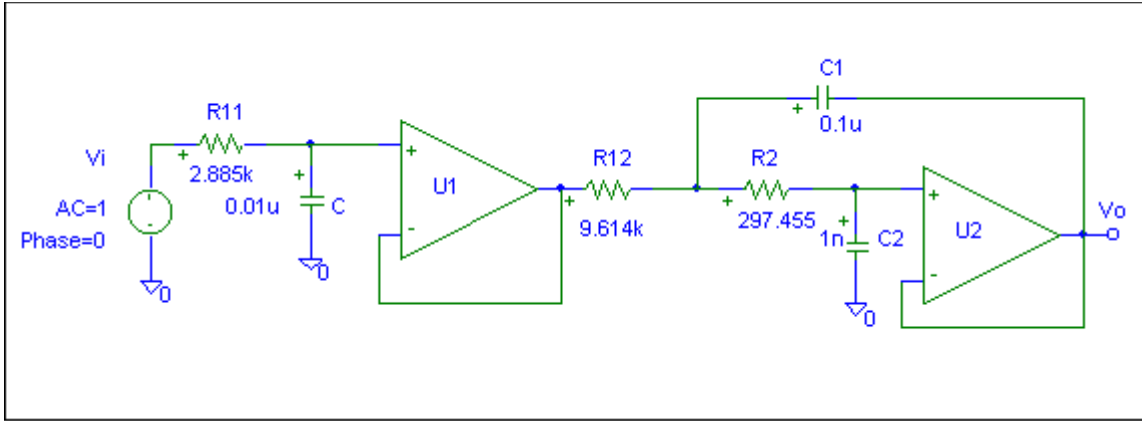
For the 2nd order filter, $K=1$, pick $R_F=0$ & R_3 open ckt.

$$f_o := f_c \cdot a_1 \quad \omega_o := 2 \cdot \pi \cdot f_o \quad Q := b_1$$

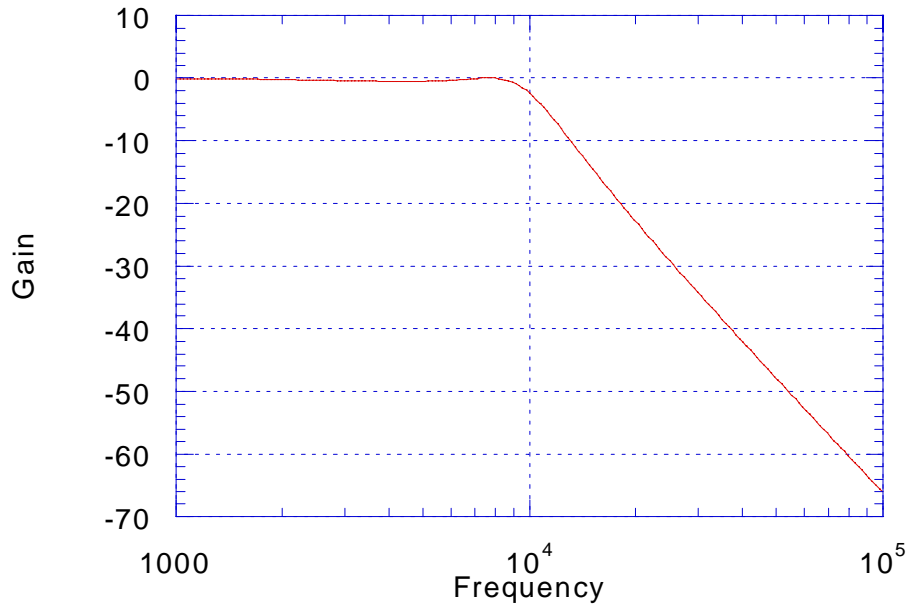
Pick $C_1 := 0.1 \mu\text{F}$ $C_2 := 0.01 \cdot C_1$

$$R_1 := \frac{1}{2 \cdot Q \cdot \omega_o \cdot C_2} \cdot \left(1 + \sqrt{1 - \frac{4 \cdot Q^2 \cdot C_2}{C_1}} \right) \quad R_1 = 9.614 \times 10^3 \Omega \quad C_1 = 1 \times 10^{-7} \text{F}$$

$$R_2 := \frac{1}{2 \cdot Q \cdot \omega_o \cdot C_2} \cdot \left(1 - \sqrt{1 - \frac{4 \cdot Q^2 \cdot C_2}{C_1}} \right) \quad R_2 = 297.455 \Omega \quad C_2 = 1 \times 10^{-9} \text{F}$$



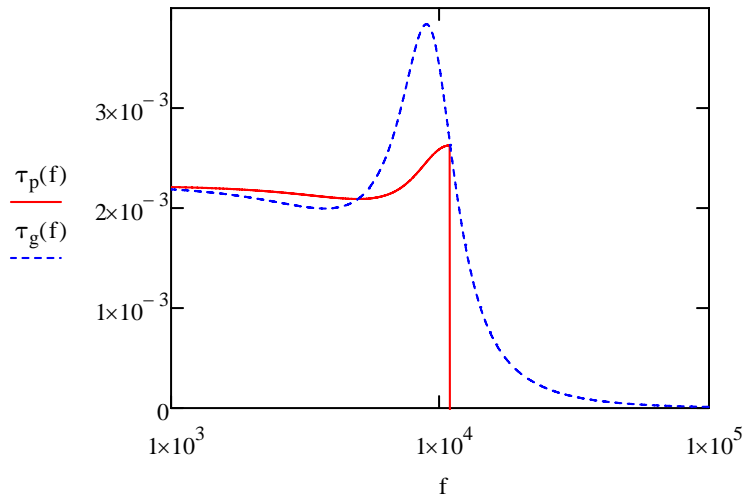
Chebyshev



$$\varphi(f) := \frac{180}{\pi} \cdot \arg(T_C(f))$$

$$\tau_p(f) := \frac{-1}{2 \cdot \pi} \cdot \frac{\varphi(f)}{f}$$

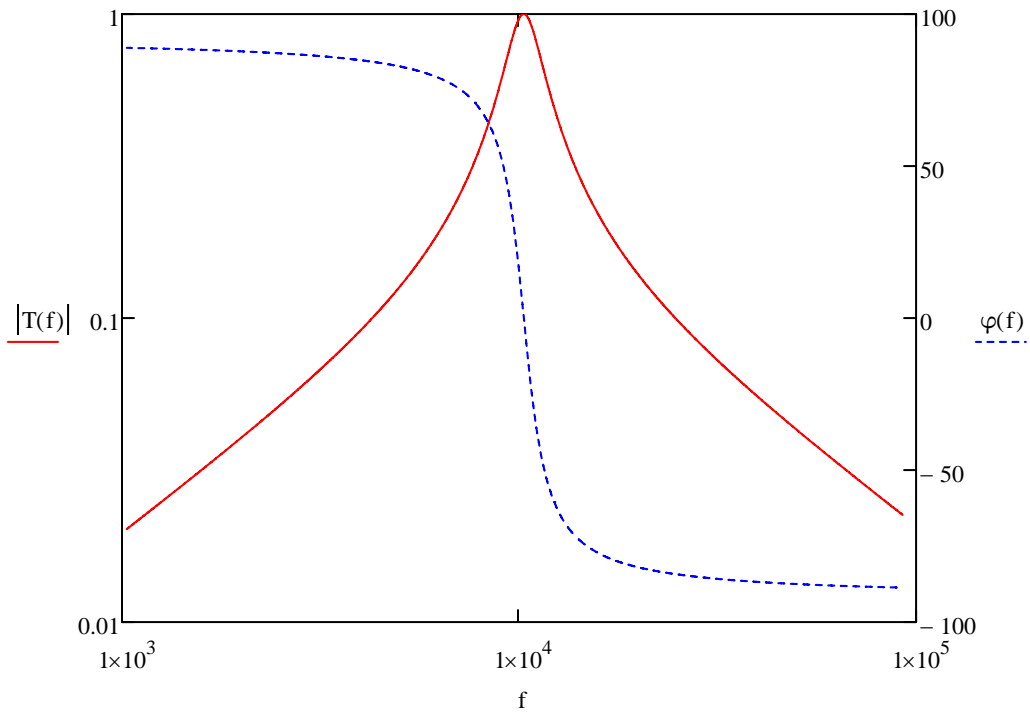
$$\tau_g(f) := \frac{-1}{2 \cdot \pi} \cdot \left(\frac{d}{df} \varphi(f) \right)$$



Second Order Sallen Key BPF

$$f_c := 10.28 \cdot \text{kHz} \quad K := 1 \quad Q := 5 \quad f_0 := f_c \quad j := \sqrt{-1}$$

$$T(f) := K \cdot \frac{\frac{1}{Q} \cdot j \cdot \frac{f}{f_0}}{\left(j \cdot \frac{f}{f_0}\right)^2 + \frac{1}{Q} \cdot j \cdot \frac{f}{f_0} + 1} \quad \varphi(f) := \frac{180}{\pi} \cdot \arg(T(f))$$



$$R_4 := 3 \cdot \text{k}\Omega \quad R_5 := 3 \cdot \text{k}\Omega \quad C_1 := 10 \cdot \text{nF} \quad C_2 := 10 \cdot \text{nF} \quad \omega_0 := 2 \cdot \pi \cdot f_0$$

$$R_1 := 1.8 \cdot \text{k}\Omega \quad R_2 := 1.8 \cdot \text{k}\Omega \quad R_3 := 1.8 \cdot \text{k}\Omega \quad K_0 := 1 + \frac{R_5}{R_4}$$

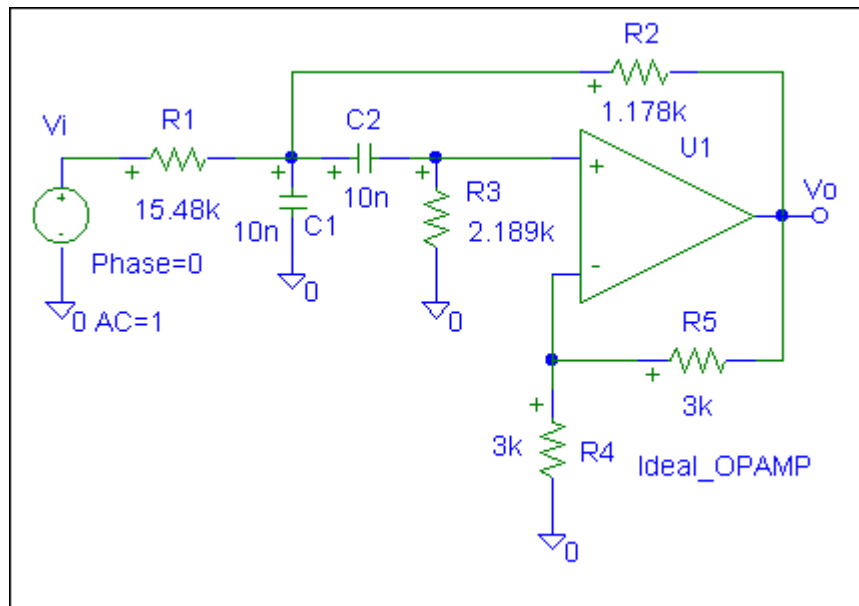
Given

$$K = \frac{R_2}{R_1 + R_2} \cdot \frac{K_0 \cdot R_3 \cdot C_2}{\left(\frac{R_1 \cdot R_2}{R_1 + R_2}\right) \cdot (C_1 + C_2) + R_3 \cdot C_2 \left[1 - \frac{K_0 \cdot R_1}{(R_1 + R_2)}\right]}$$

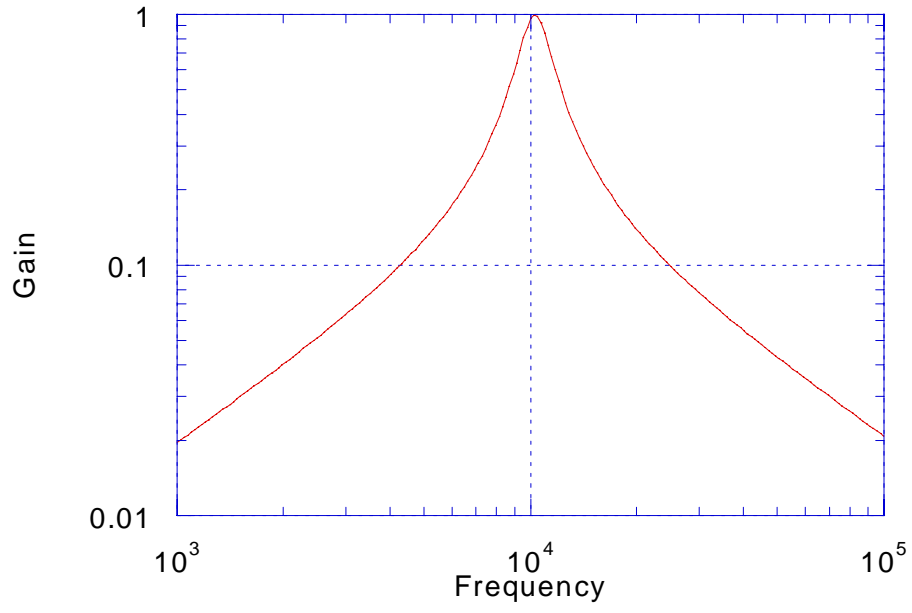
$$\omega_0 = \frac{1}{\sqrt{\frac{R_1 \cdot R_2}{R_1 + R_2} \cdot R_3 \cdot C_1 \cdot C_2}}$$

$$Q = \frac{\sqrt{\frac{R_1 \cdot R_2}{R_1 + R_2} \cdot R_3 \cdot C_1 \cdot C_2}}{\left(\frac{R_1 \cdot R_2}{R_1 + R_2}\right)(C_1 + C_2) + R_3 \cdot C_2 \cdot \left(1 - \frac{K_o \cdot R_1}{R_1 + R_2}\right)}$$

$$\text{Find}(R_1, R_2, R_3) = \begin{pmatrix} 1.548 \times 10^4 \\ 1.178 \times 10^3 \\ 2.189 \times 10^3 \end{pmatrix} \Omega$$



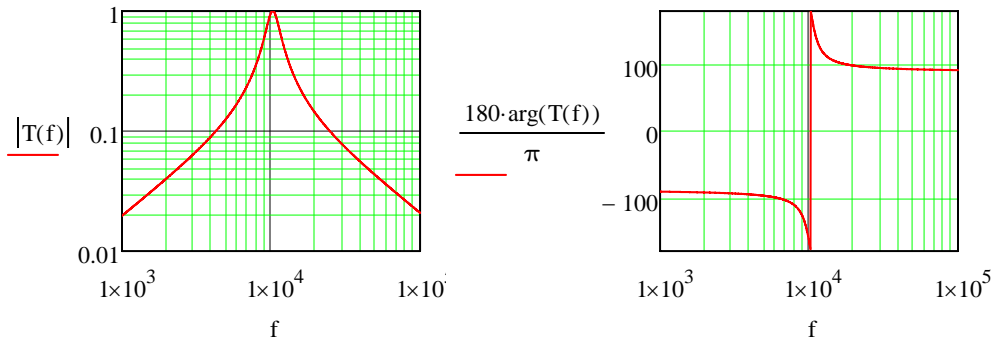
Sallen Key BPF



Second Order Infinite Gain Multiple Feedback BPF, page 87, Exp 6

$$f_0 := 10.28 \cdot \text{kHz} \quad Q := 5 \quad K := 1 \quad \omega_0 := 2 \cdot \pi \cdot f_0 \quad j := \sqrt{-1}$$

$$T(f) := -K \frac{\frac{1}{Q} \cdot j \cdot \frac{f}{f_0}}{\left(j \cdot \frac{f}{f_0}\right)^2 + \frac{1}{Q} \cdot j \cdot \frac{f}{f_0} + 1}$$



$$C_1 := 0.01 \cdot \mu\text{F} \quad C_2 := C_1 \quad R_1 := 10 \cdot \text{k}\Omega \quad R_2 := 240 \cdot \Omega \quad R_3 := 20 \cdot \text{k}\Omega$$

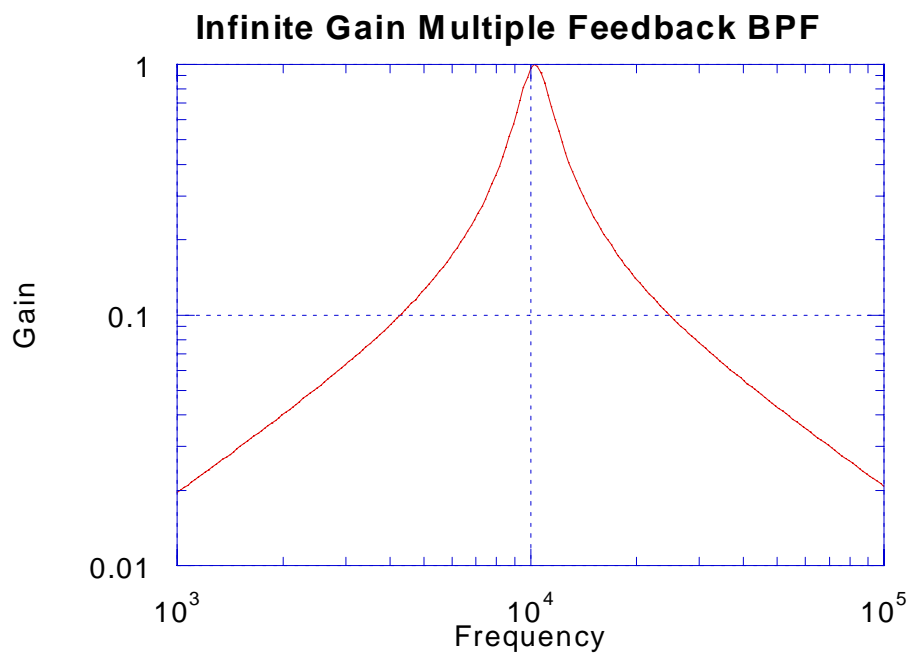
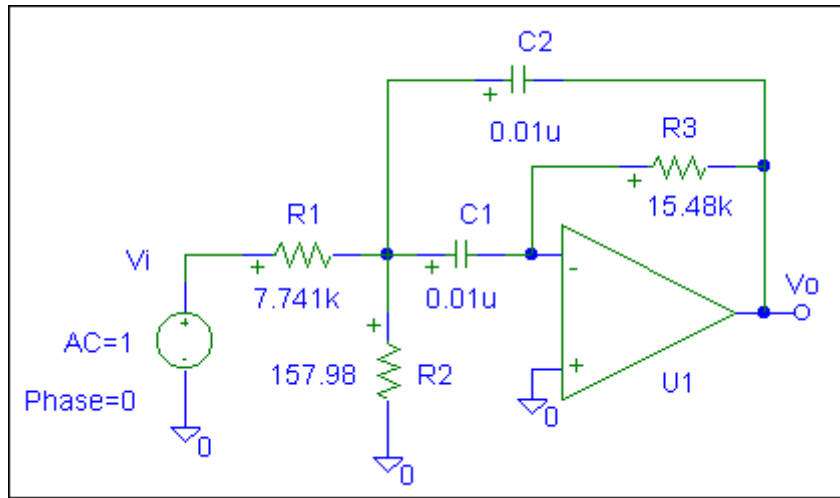
Given

$$\frac{R_3 \cdot C_1}{R_1 \cdot (C_1 + C_2)} = K$$

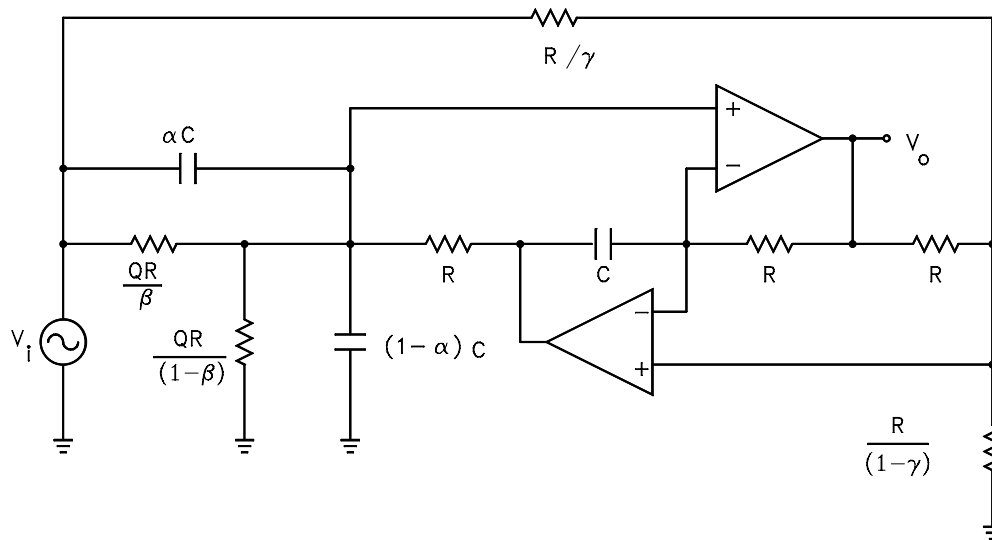
$$\frac{1}{\sqrt{\frac{R_1 \cdot R_2 \cdot R_3 \cdot C_1 \cdot C_2}{R_1 + R_2}}} = \omega_0$$

$$\frac{\sqrt{\frac{R_3 \cdot C_1 \cdot C_2 \cdot (R_1 + R_2)}{(R_1 \cdot R_2)}}}{C_1 + C_2} = Q$$

$$\text{Find}(R_1, R_2, R_3) = \begin{pmatrix} 7.741 \times 10^3 \\ 157.98 \\ 1.548 \times 10^4 \end{pmatrix} \Omega$$



General Bi Quadratic Filter



$$T(s) = \left[\frac{\left(\frac{s}{\omega_o}\right)^2 \cdot (2 \cdot \alpha - \gamma) + \frac{1}{Q} \cdot \left(\frac{s}{\omega_o}\right) \cdot (2 \cdot \beta - \gamma) + \gamma}{\left(\frac{s}{\omega_o}\right)^2 + \frac{1}{Q} \cdot \frac{s}{\omega_o} + 1} \right]$$

$$f_o := 10.28\text{kHz} \quad N := 2000 \quad i := 0..N-1 \quad f_{\text{start}} := 1\text{kHz} \quad j := \sqrt{-1}$$

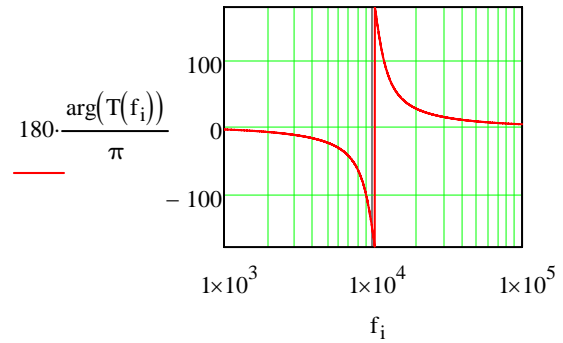
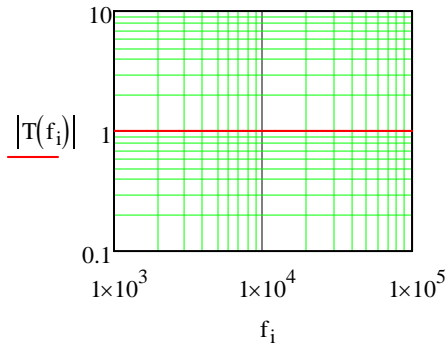
$$f_{\text{stop}} := 100\text{kHz}$$

$$f_i := f_{\text{start}} \cdot \left(\frac{f_{\text{stop}}}{f_{\text{start}}} \right)^{\frac{i}{N-1}}$$

Allpass

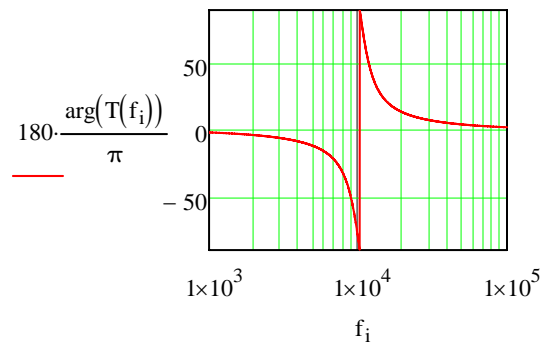
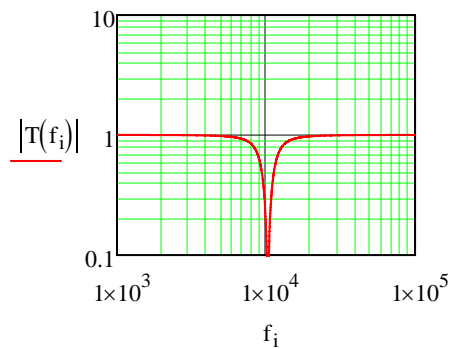
$$Q := 3 \quad \alpha := 1 \quad \beta := 0 \quad \gamma := 1$$

$$T(f) := \frac{\left(\frac{f}{f_o} \cdot j\right)^2 \cdot (2 \cdot \alpha - \gamma) + \frac{1}{Q} \cdot \left(\frac{j \cdot f}{f_o}\right) \cdot (2 \cdot \beta - \gamma) + \gamma}{\left(j \cdot \frac{f}{f_o}\right)^2 + \frac{1}{Q} \cdot \frac{j \cdot f}{f_o} + 1}$$



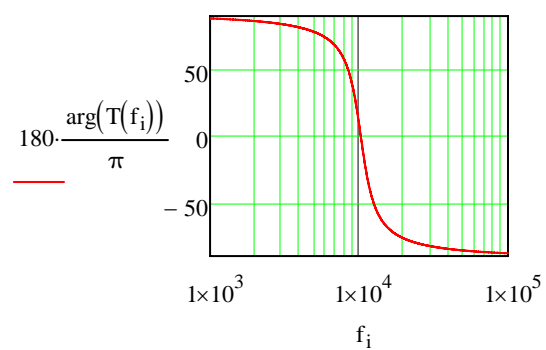
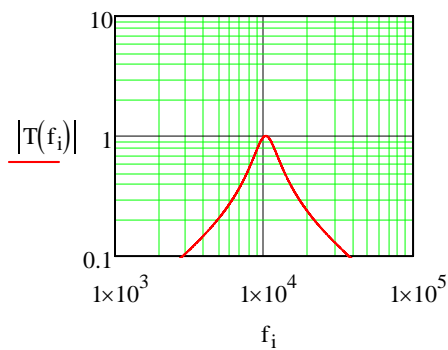
Notch $\alpha := 1$ $\beta := 0.5$ $\gamma := 1$ $Q := 3$ $f_o := 10.28\text{kHz}$

$$T(f) := \frac{\left(\frac{f}{f_o} \cdot j\right)^2 \cdot (2 \cdot \alpha - \gamma) + \frac{1}{Q} \cdot \left(\frac{j \cdot f}{f_o}\right) \cdot (2 \cdot \beta - \gamma) + \gamma}{\left(j \frac{f}{f_o}\right)^2 + \frac{1}{Q} \cdot \frac{j \cdot f}{f_o} + 1}$$



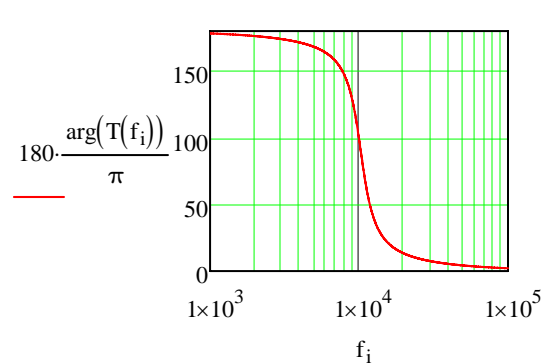
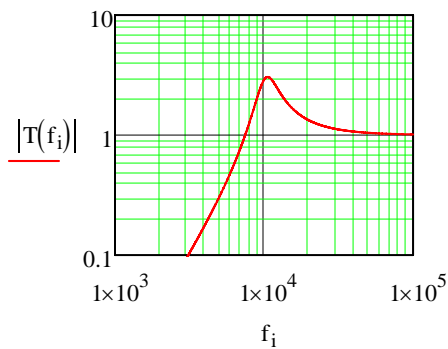
Bandpass $\alpha := 0$ $\beta := 0.5$ $\gamma := 0$ $f_o := 10.28\text{kHz}$ $Q := 3$

$$T(f) := \frac{\left(\frac{f}{f_0} \cdot j\right)^2 \cdot (2 \cdot \alpha - \gamma) + \frac{1}{Q} \cdot \left(\frac{j \cdot f}{f_0}\right) \cdot (2 \cdot \beta - \gamma) + \gamma}{\left(j \frac{f}{f_0}\right)^2 + \frac{1}{Q} \cdot \frac{j \cdot f}{f_0} + 1}$$



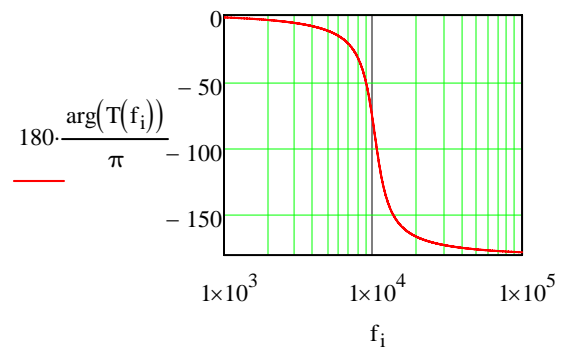
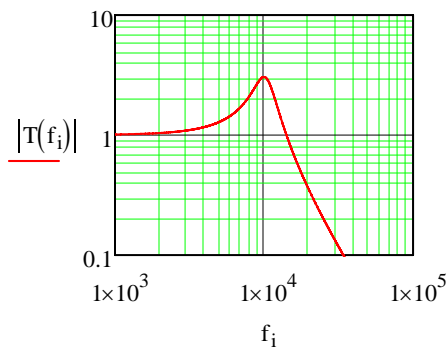
Highpass $\alpha := 0.5$ $\beta := 0$ $\gamma := 0$ $f_0 := 10.28\text{kHz}$ $Q := 3$

$$T(f) := \frac{\left(\frac{f}{f_0} \cdot j\right)^2 \cdot (2 \cdot \alpha - \gamma) + \frac{1}{Q} \cdot \left(\frac{j \cdot f}{f_0}\right) \cdot (2 \cdot \beta - \gamma) + \gamma}{\left(j \frac{f}{f_0}\right)^2 + \frac{1}{Q} \cdot \frac{j \cdot f}{f_0} + 1}$$



Lowpass $\alpha := 0.5$ $\beta := 0.5$ $\gamma := 1$ $f_o := 10.28\text{kHz}$ $Q := 3$

$$T(f) := \frac{\left(\frac{f}{f_o} \cdot j\right)^2 \cdot (2 \cdot \alpha - \gamma) + \frac{1}{Q} \cdot \left(\frac{j \cdot f}{f_o}\right) \cdot (2 \cdot \beta - \gamma) + \gamma}{\left(j \frac{f}{f_o}\right)^2 + \frac{1}{Q} \cdot \frac{j \cdot f}{f_o} + 1}$$



Third Order Elliptic Filter with 0.5 db ripple unity dc gain with stop band to cutoff ratio of 1.5

with a min attenuation in the stop band of 21.9 dB from page 79 in the lab manual

$$T(s) = \frac{1}{\frac{s}{0.76695 \omega_c} + 1} \cdot \frac{\left(\frac{s}{1.6751 \cdot \omega_c}\right)^2 + 1}{\left(\frac{s}{1.0720 \cdot \omega_c}\right)^2 + \frac{1}{2.3672} \cdot \frac{s}{1.0720 \cdot \omega_c} + 1}$$

this requires that a first order filter be cascaded with a bi quad
for a notch at fp this means

$$f_c := 10.28\text{kHz} \quad \gamma := 1 \quad \beta := \frac{1}{2} \quad f_o := 1.072 \cdot f_c$$

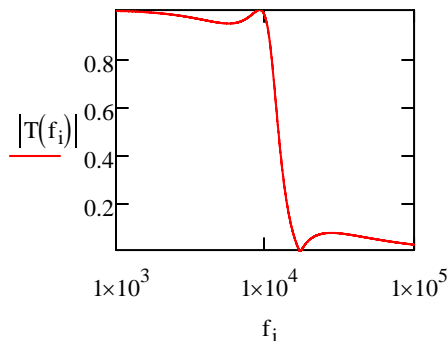
$$\alpha := \frac{\gamma + \left(\frac{1.072}{1.6751}\right)^2}{2} = 0.705 \quad Q := 2.3672$$

$$T_2(f) := \frac{\left(\frac{f}{f_o} \cdot j\right)^2 \cdot (2 \cdot \alpha - \gamma) + \frac{1}{Q} \cdot \left(\frac{j \cdot f}{f_o}\right) \cdot (2 \cdot \beta - \gamma) + \gamma}{\left(j \frac{f}{f_o}\right)^2 + \frac{1}{Q} \cdot \frac{j \cdot f}{f_o} + 1}$$

for the first order filter

$$f_1 := 0.7669 \cdot f_c$$

$$T_1(f) := \frac{1}{1 + j \cdot \frac{f}{f_1}} \quad T(f) := T_1(f) \cdot T_2(f)$$

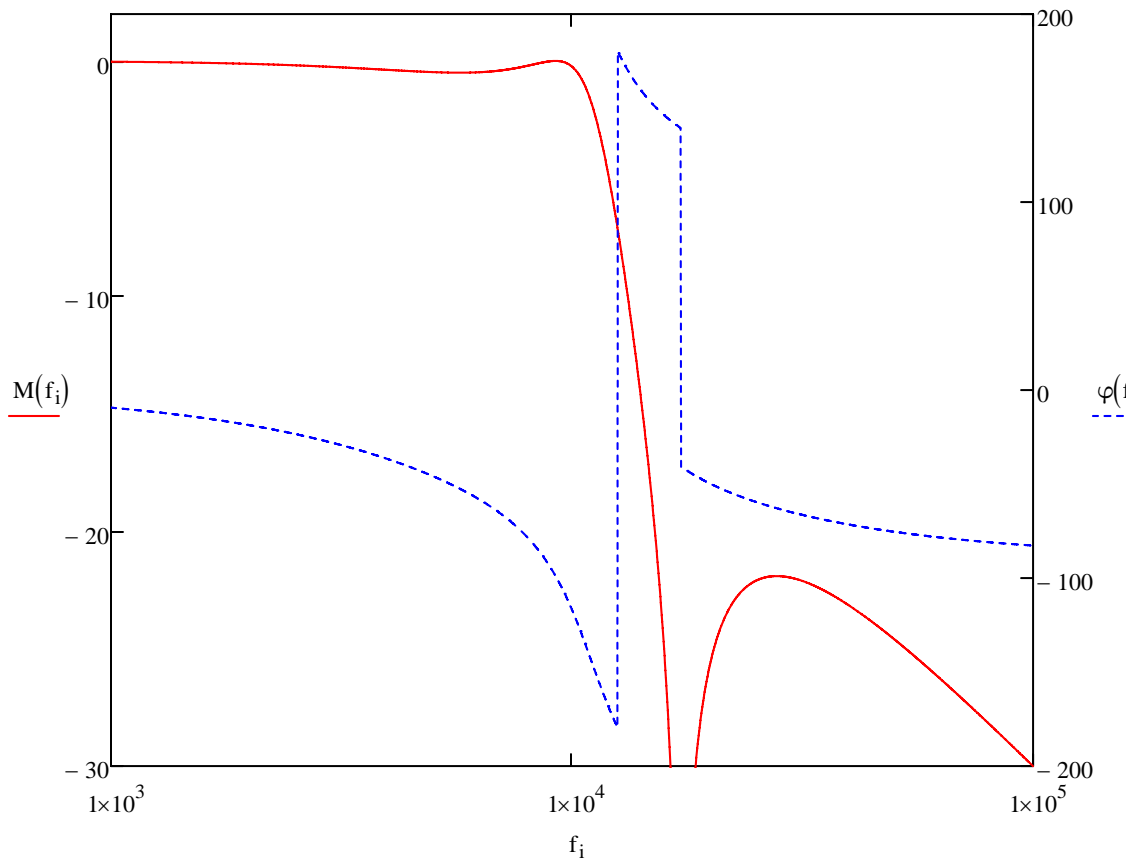


$$\varphi(f) := \frac{180}{\pi} \cdot \arg(T(f))$$

$$\tau_g(f) := -\frac{1}{2 \cdot \pi} \cdot \left(\frac{d}{df} \varphi(f)\right)$$

$$\tau_p(f) := -\frac{\varphi(f)}{2 \cdot \pi \cdot f}$$

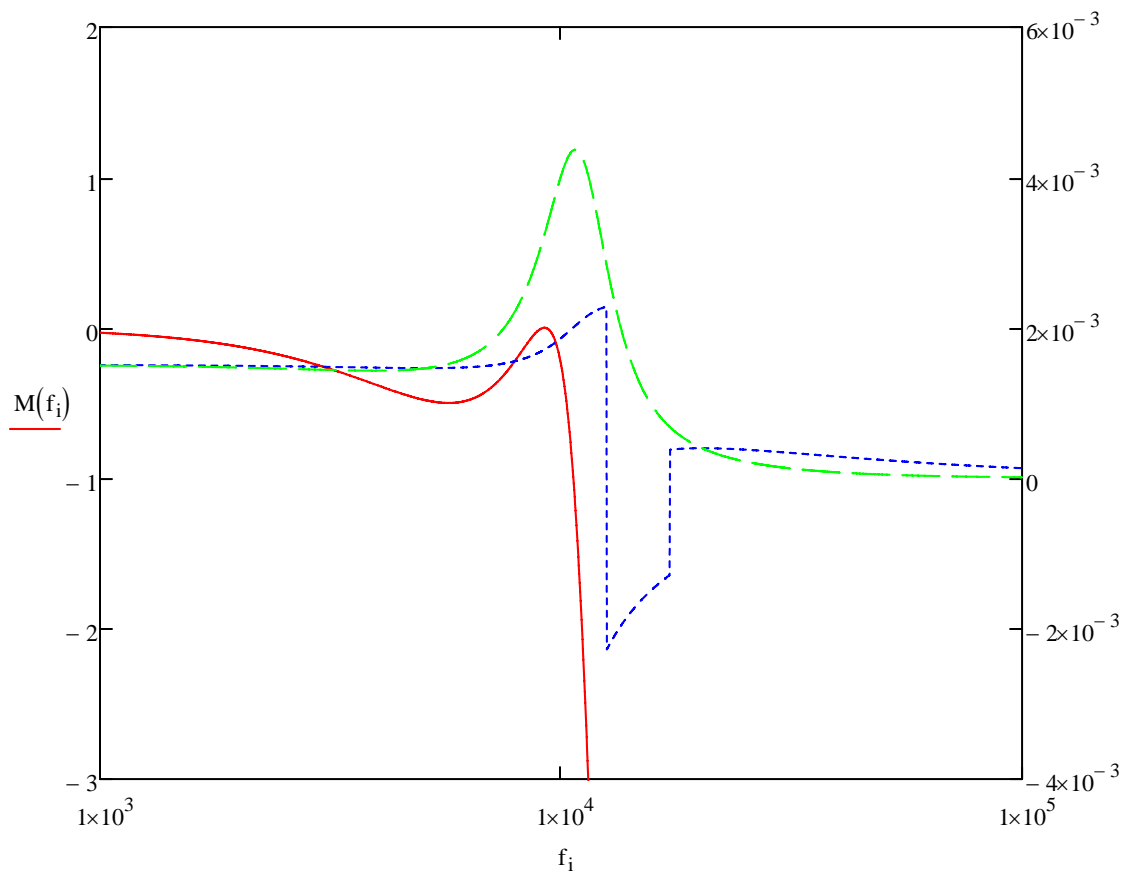
$$M(f) := 20 \cdot \log(|T(f)|)$$



$$\varphi(f) := \frac{180}{\pi} \cdot \arg(T(f))$$

$$\tau_p(f) := -\frac{\varphi(f)}{2 \cdot \pi \cdot f}$$

$$\tau_g(f) := -\frac{1}{2 \cdot \pi} \cdot \left(\frac{d}{df} \varphi(f) \right)$$



Third Order Bessel Filter

$$f_3 := 10.28\text{kHz}$$

$$f_c := \frac{f_3}{1.7557}$$

$$a_2 := 2.3222$$

$$a_1 := 2.5415$$

$$b_1 := 0.69105$$

$$T(f) := \frac{1}{j \cdot \frac{f}{a_2 \cdot f_c} + 1} \cdot \frac{1}{\left(j \cdot \frac{f}{a_1 \cdot f_c} \right)^2 + \frac{1}{b_1} \cdot j \cdot \frac{f}{a_1 \cdot f_c} + 1}$$

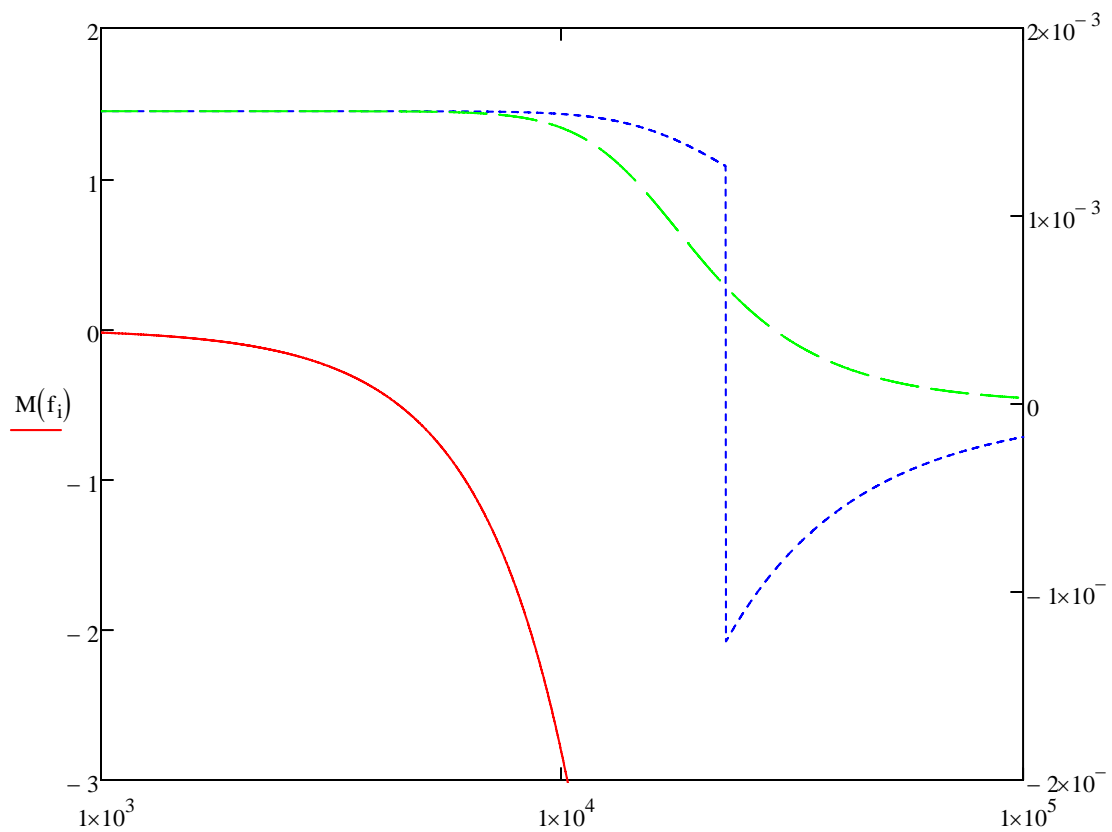
$$M(f) := 20 \cdot \log(|T(f)|)$$

$$\varphi(f) := \frac{180}{\pi} \cdot \arg(T(f))$$

$$\varphi(f) := \frac{180}{\pi} \cdot \arg(T(f))$$

$$\tau_p(f) := -\frac{\varphi(f)}{2 \cdot \pi \cdot f}$$

$$\tau_g(f) := -\frac{1}{2 \cdot \pi} \cdot \left(\frac{d}{df} \varphi(f) \right)$$



f_i

$$n = 3 \quad \frac{f_3}{f_c} = 1.7557 \quad a_1 := 2.5415 \quad b_1 := 0.69105$$
$$a_2 := 2.3222$$

$$T(s) = \frac{1}{\frac{s}{a_2 \cdot \omega_c} + 1} \cdot \frac{1}{\left(\frac{s}{a_1 \cdot \omega_c}\right)^2 + \frac{1}{b_1} \cdot \frac{s}{a_1 \cdot \omega_c} + 1}$$

1st Order LPF
2nd Order LPF

$$f_3 := 10.28\text{kHz} \quad f_c := \frac{f_3}{1.7557} \quad \omega_c := 2 \cdot \pi \cdot f_c$$

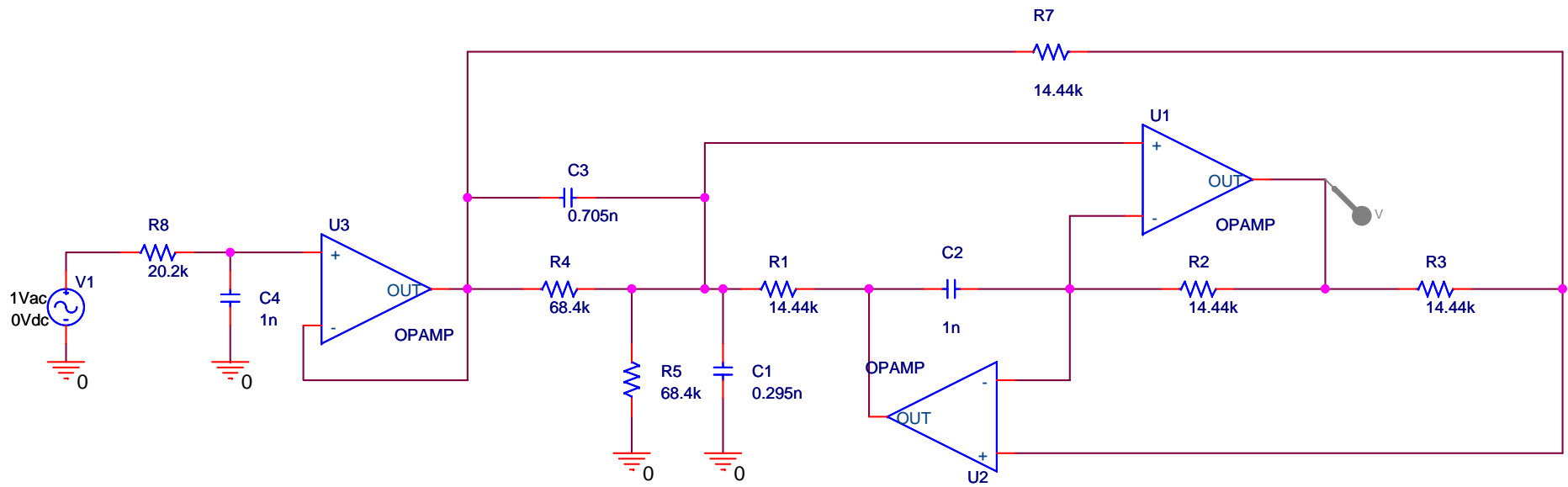
$$C_3 := 1\text{nF} \quad R_3 := \frac{1}{a_2 \cdot \omega_c \cdot C_3} = 1.171 \times 10^4 \Omega$$

Use Sallen Key

$$C_1 := 0.01\mu\text{F} \quad C_2 := 0.1 \cdot C_1$$

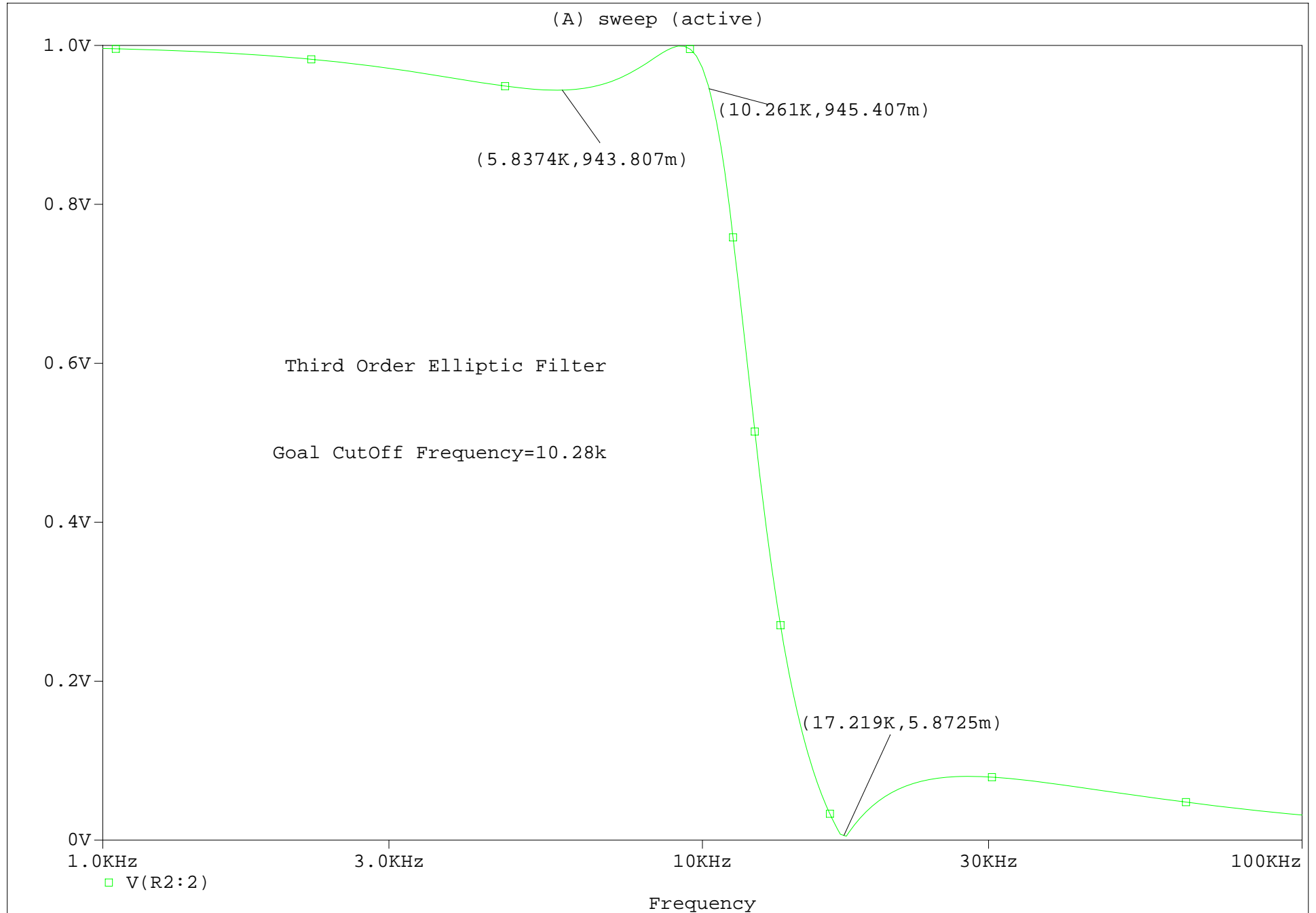
$$R_1 := \frac{1}{2 \cdot b_1 \cdot a_1 \cdot \omega_c \cdot C_2} \cdot \left(1 + \sqrt{1 - 4 \cdot b_1^2 \cdot \frac{C_2}{C_1}}\right) = 1.47 \times 10^4 \Omega$$

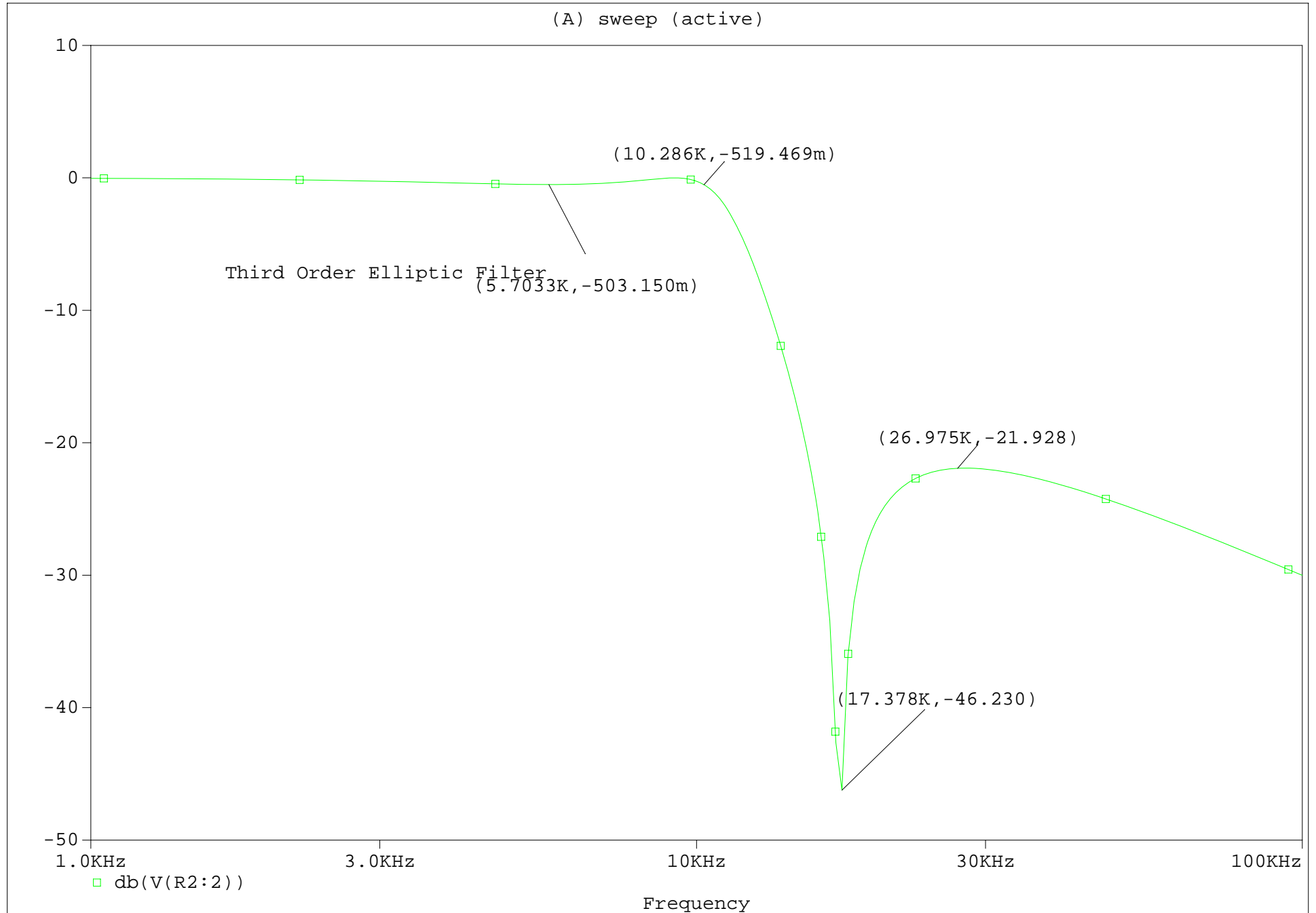
$$R_2 := \frac{1}{2 \cdot b_1 \cdot a_1 \cdot \omega_c \cdot C_2} \cdot \left(1 - \sqrt{1 - 4 \cdot b_1^2 \cdot \frac{C_2}{C_1}}\right) = 778.221 \Omega$$

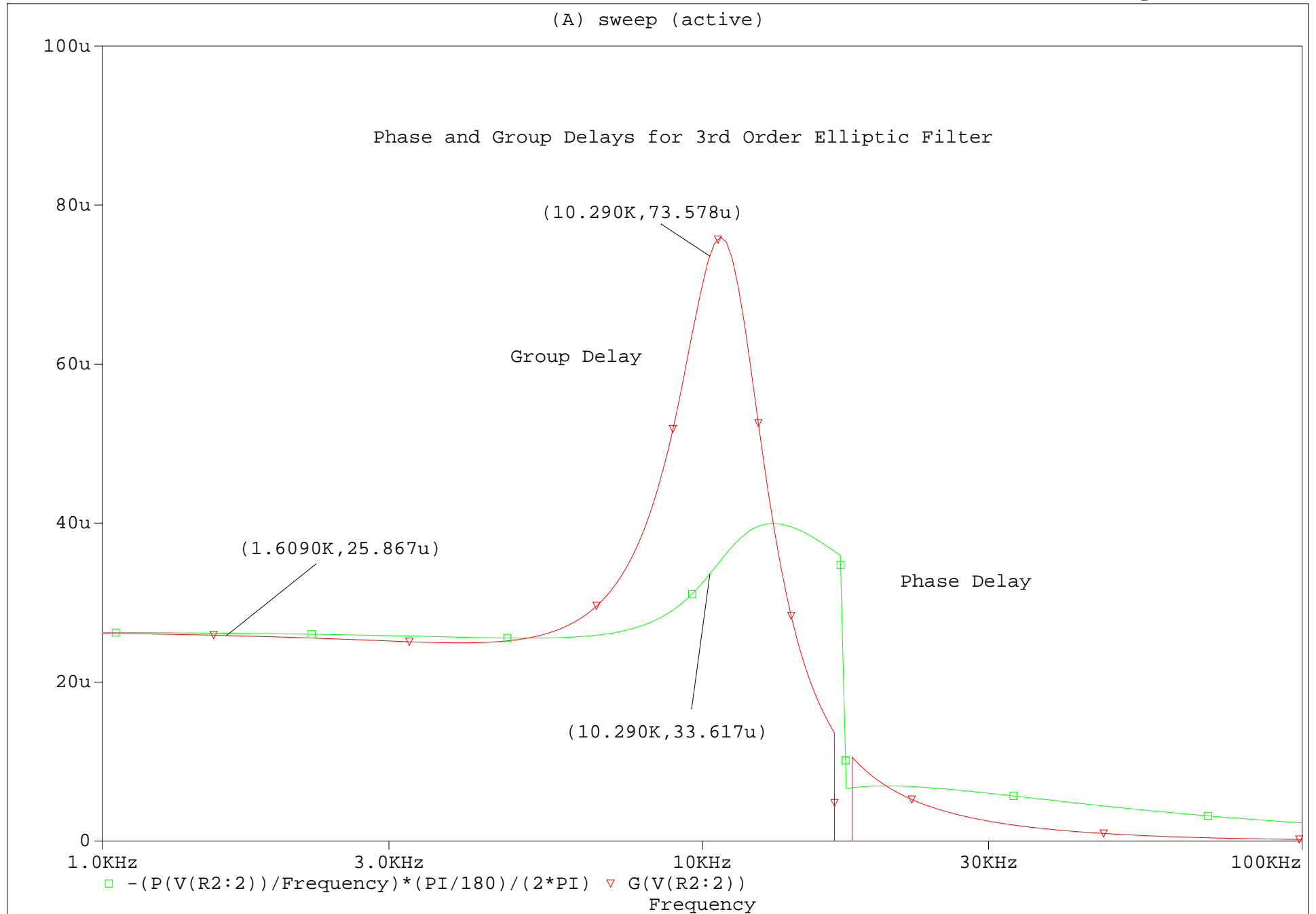


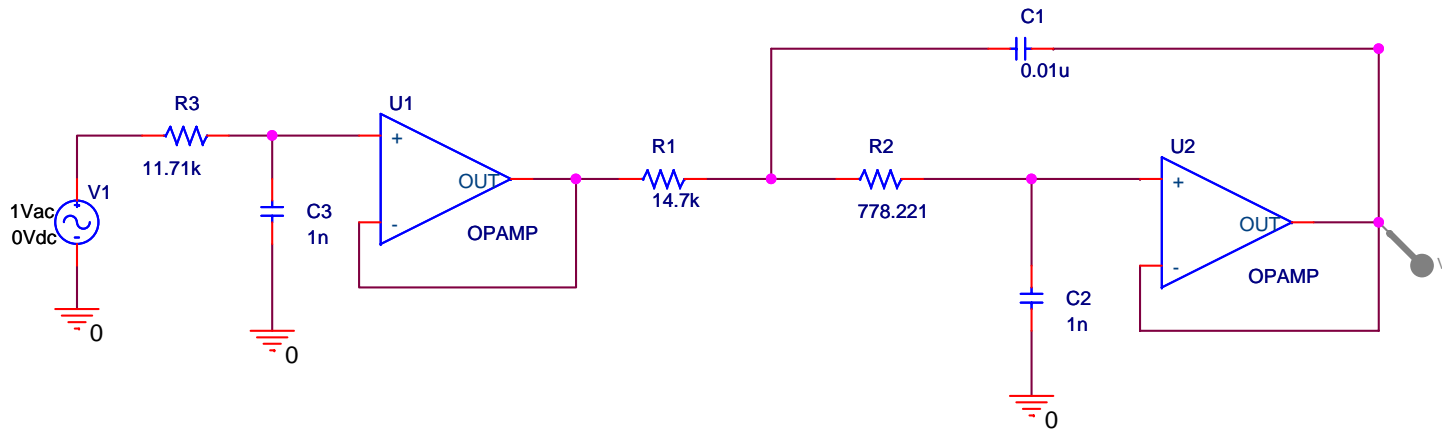
Third Order Elliptic Filter

Title		
Third Order Elliptic Filter		
Size	Document Number	Rev
A	Active Filters	1
Date:	Tuesday, March 11, 2008	Sheet 1 of 1



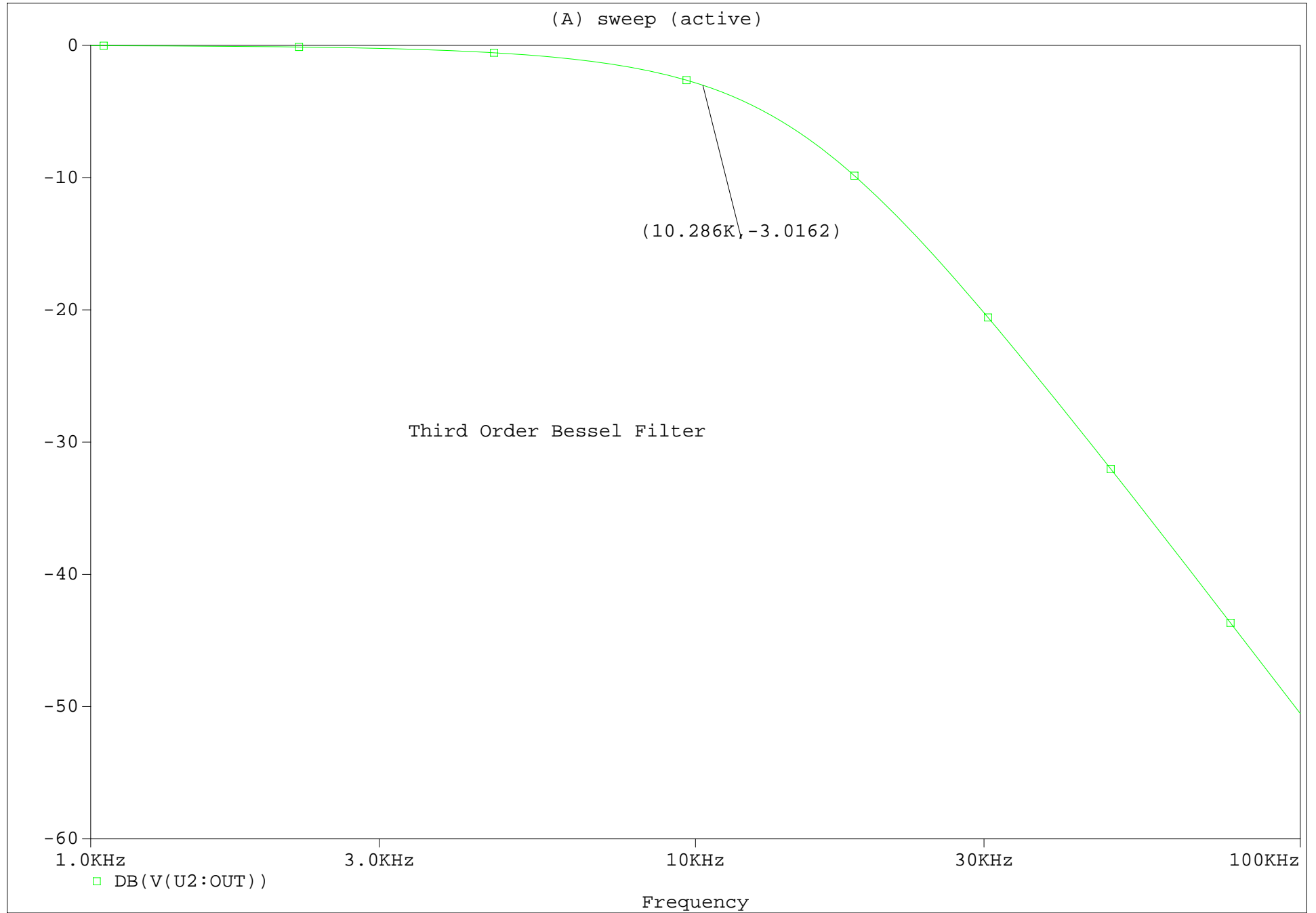


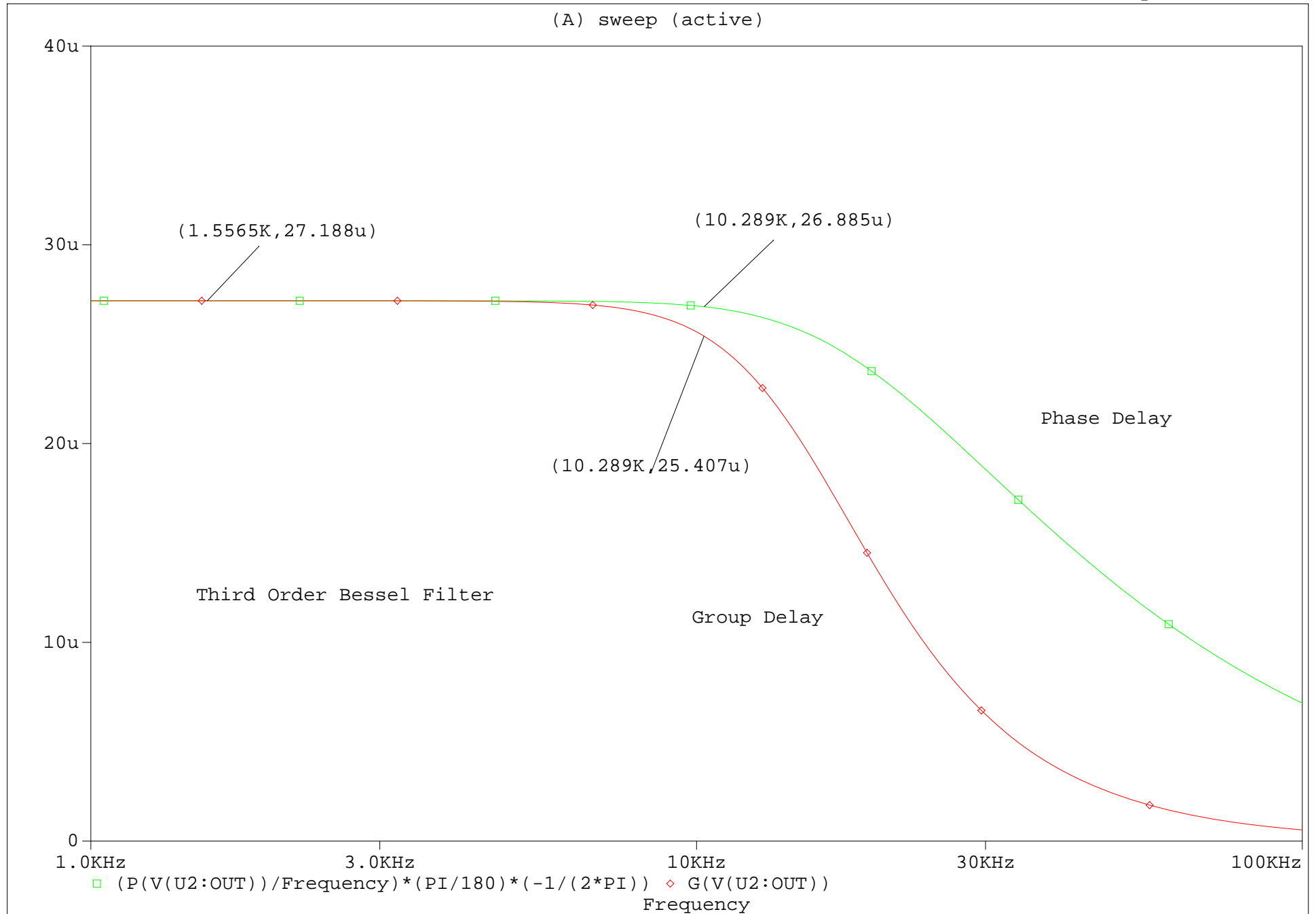




Third Order Bessel Filter

Title		
Third Order Bessel Filter		
Size	Document Number	Rev
A	Active Filters	1
Date:	Wednesday, March 12, 2008	Sheet 1 of 1





Georgia Institute of Technology

School of Electrical and Computer Engineering

ECE 3042

Microelectronic Circuits Laboratory

Verification Sheet

NAME: _____

SECTION: _____

GT NUMBER: _____

GTID: _____

Experiment 6: Op-Amp Active Filters

Procedure	Time Completed	Date Completed	Verification (Must demonstrate circuit)	Points Possible	Points Received
1. Third-Order Butterworth LPF				16	
2. Third-Order Chebyshev LPF				16	
3. Second-Order Band-Pass				16	
4. Second-Order Notch				16	
5. First-Order All-Pass				16	
6. Second-Order All-Pass				20	

Enter your critical frequency below:

f_{crit}	
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To be permitted to complete the experiment during the open lab hours, you must complete at least **three** procedures during your scheduled lab period or spend your entire scheduled lab session attempting to do so. A signature below by your lab instructor, Dr. Brewer, or Dr. Robinson permits you to attend the open lab hours to complete the experiment and receive full credit on the report. Without this signature, you may use the open lab to perform the experiment at a 50% penalty.

SIGNATURE: _____

DATE: _____

ECE 3042 Check-off Requirements for Experiment 6

Make sure you have made all required measurements before requesting a check-off. For all check-offs, you must demonstrate the circuit or measurement to a lab instructor. All screen captures must have a time/date stamp.

Do not follow the procedures in the lab manual. Only Bode magnitude plots are required—it is not necessary to measure the phase. Do not follow the lab report format for this experiment. Instead, display two Bode plots and their associated tables per page.

1. Third-Order Butterworth Low-Pass Filter

- ✓ Bode gain magnitude plot over frequency range of 100Hz to 100kHz.
- ✓ Measurement of dc gain and -3dB frequency.
- ✓ Table comparing these measured values to the design specifications. Show percent error.

2. Third-Order Chebyshev Low-Pass Filter

- ✓ Bode gain magnitude plot over frequency range of 100Hz to 100kHz.
- ✓ Measurement of dc gain, dB ripple, and -3dB frequency.
- ✓ Table comparing these measured values to the design specifications. Show percent error.

3. Second-Order Bandpass Filter

- ✓ Bode gain magnitude plot over frequency range of 100Hz to 100kHz.
- ✓ Measurement of center frequency f_o , -3dB bandwidth BW, and Q. Q is given by f_o / BW .
- ✓ Table comparing these measured values to the design specifications. Show percent error.

4. Second-Order Notch Filter

- Implement filter with the general biquad circuit from the class notes. Save this filter—it can be modified to obtain the second-order all-pass transfer function.
- ✓ Bode gain magnitude plot over frequency range of 100Hz to 100kHz.
- ✓ Measurement of center frequency f_o , -3dB bandwidth BW, and Q. Q is given by f_o / BW .
- ✓ Table comparing these measured values to the design specifications. Show percent error.

5. First-Order All-Pass Filter

- ✓ Bode gain magnitude plot over frequency range of 100Hz to 100kHz.
- ✓ Measurement of dc gain.
- ✓ Scope screen capture showing measured f_{crit} , the frequency at which the phase shift between input and output is 90 deg. Connect input to ch1 and output to ch2. Display measured Vpp for each channel, the frequency, and the phase.
- ✓ Table comparing these measured values to the design specifications. Show percent error.

6. Second-Order All-Pass Filter

- ✓ Bode gain magnitude plot over frequency range of 100Hz to 100kHz.
- ✓ Measurement of dc gain.
- ✓ Scope screen capture showing measured f_{crit} , the frequency at which the phase shift between input and output is 180 deg. Connect input to ch1 and output to ch2. Display measured Vpp for each channel, the frequency, and the phase.
- ✓ Table comparing these measured values to the design specifications. Show percent error.